



Lattice Imperfections and Off-momentum Particles



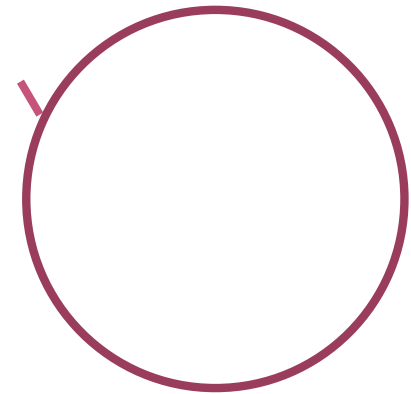
Lattice Imperfections

- Up until now, we have considered an ideal lattice, but real magnets aren't perfect.
- We will consider two types of lattice imperfections:
 - ◆ Dipole errors
 - ◆ Quadrupole errors
- We will also discuss how to locally correct the position of the beam.



Closed Orbit Distortion (“cusp”)

- We place a dipole at one point in a ring which bends the beam by an amount Θ .
- The new equilibrium orbit will be defined by a trajectory which goes once around the ring, through the dipole, and then returns to its exact initial conditions. That is



$$\mathbf{M} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix} + \begin{pmatrix} 0 \\ \theta \end{pmatrix} = \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix} \Rightarrow (\mathbf{I} - \mathbf{M}) \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix} = \begin{pmatrix} 0 \\ \theta \end{pmatrix}$$

$$\Rightarrow \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix} = (\mathbf{I} - \mathbf{M})^{-1} \begin{pmatrix} 0 \\ \theta \end{pmatrix}$$

- Recall that we can express the transfer matrix for a complete revolution as

$$\mathbf{M}(s+C, s) = \begin{pmatrix} \cos 2\pi\nu + \alpha(s) \sin 2\pi\nu & \beta(s) \sin 2\pi\nu \\ -\gamma(s) \sin 2\pi\nu & \cos 2\pi\nu - \alpha(s) \sin 2\pi\nu \end{pmatrix} = \mathbf{I} \cos 2\pi\nu + \mathbf{J} \sin 2\pi\nu = e^{\mathbf{J}2\pi\nu}$$

$$(\mathbf{I} - \mathbf{M}) = e^{\mathbf{J}\pi\nu} (e^{-\mathbf{J}\pi\nu} - e^{\mathbf{J}\pi\nu}) = -e^{\mathbf{J}\pi\nu} (2 \sin \pi\nu \mathbf{J})$$

$$(\mathbf{I} - \mathbf{M})^{-1} = (-2 \sin \pi\nu \mathbf{J})^{-1} (e^{\mathbf{J}\pi\nu})^{-1}$$

$$= \frac{1}{2 \sin \pi\nu} \mathbf{J} e^{-\mathbf{J}\pi\nu} = \frac{1}{2 \sin \pi\nu} \mathbf{J} (\mathbf{I} \cos \pi\nu - \mathbf{J} \sin \pi\nu)$$

$$= \frac{1}{2 \sin \pi\nu} (\mathbf{J} \cos \pi\nu + \mathbf{I} \sin \pi\nu)$$

$$= \frac{1}{2 \sin \pi\nu} \begin{pmatrix} \alpha \cos \pi\nu + \sin \pi\nu & \beta \cos \pi\nu \\ -\gamma \cos \pi\nu & -\alpha \cos \pi\nu + \sin \pi\nu \end{pmatrix}$$

$$\mathbf{J} \equiv \begin{pmatrix} \alpha & \beta \\ -\gamma & -\alpha \end{pmatrix}$$

$$\mathbf{J}^2 = -\mathbf{I}$$

$$\mathbf{J}^{-1} = -\mathbf{J}$$



➤ Plug this back in
$$\begin{pmatrix} x_0 \\ x'_0 \end{pmatrix} = \frac{1}{2 \sin \pi \nu} \begin{pmatrix} \alpha \cos \pi \nu + \sin \pi \nu & \beta \cos \pi \nu \\ -\gamma \cos \pi \nu & -\alpha \cos \pi \nu + \sin \pi \nu \end{pmatrix} \begin{pmatrix} 0 \\ \theta \end{pmatrix}$$
$$= \frac{\theta}{2 \sin \pi \nu} \begin{pmatrix} \beta_0 \cos \pi \nu \\ \sin \pi \nu - \alpha_0 \cos \pi \nu \end{pmatrix}$$

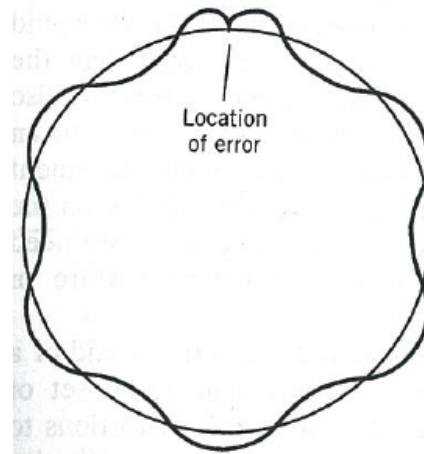
➤ We now propagate this around the ring

$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = \frac{\theta}{2 \sin \pi \nu} \begin{pmatrix} \sqrt{\frac{\beta(s)}{\beta_0}} (\cos \Delta \psi + \alpha_0 \sin \Delta \psi) & \sqrt{\beta_0 \beta(s)} \sin \Delta \psi \\ \frac{1}{\sqrt{\beta_0 \beta(s)}} ((\alpha_0 - \alpha(s)) \cos \Delta \psi - (1 + \alpha_0 \alpha(s)) \sin \Delta \psi) & \sqrt{\frac{\beta_0}{\beta(s)}} (\cos \Delta \psi - \alpha(s) \sin \Delta \psi) \end{pmatrix} \begin{pmatrix} \beta_0 \cos \pi \nu \\ \sin \pi \nu - \alpha_0 \cos \pi \nu \end{pmatrix}$$

$$\Rightarrow x(s) = \frac{\theta}{2 \sin \pi \nu} \left(\sqrt{\frac{\beta(s)}{\beta_0}} (\cos \Delta \psi + \alpha_0 \sin \Delta \psi) \beta_0 \cos \pi \nu + \sqrt{\beta_0 \beta(s)} \sin \Delta \psi (\sin \pi \nu - \alpha_0 \cos \pi \nu) \right)$$

$$= \frac{\theta \sqrt{\beta_0 \beta(s)}}{2 \sin \pi \nu} (\cos \Delta \psi \cos \pi \nu + \sin \Delta \psi \cos \pi \nu)$$

$$= \frac{\theta \sqrt{\beta_0 \beta(s)}}{2 \sin \pi \nu} \cos(\Delta \psi - \pi \nu)$$





Quadrupole Errors

- We can express the matrix for a complete revolution at a point as

$$\mathbf{M}(s) = \begin{pmatrix} \cos 2\pi\nu + \alpha(s) \sin 2\pi\nu & \beta(s) \sin 2\pi\nu \\ -\gamma(s) \sin 2\pi\nu & \cos 2\pi\nu - \alpha(s) \sin 2\pi\nu \end{pmatrix}$$

- If we add focusing quad at this point, we have

$$\begin{aligned} \mathbf{M}'(s) &= \begin{pmatrix} \cos 2\pi\nu_0 + \alpha(s) \sin 2\pi\nu_0 & \beta(s) \sin 2\pi\nu_0 \\ -\gamma(s) \sin 2\pi\nu_0 & \cos 2\pi\nu - \alpha(s) \sin 2\pi\nu_0 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{pmatrix} \\ &= \begin{pmatrix} \cos 2\pi\nu_0 + \alpha(s) \sin 2\pi\nu_0 - \frac{\beta(s)}{f} \sin 2\pi\nu_0 & \beta(s) \sin 2\pi\nu_0 \\ -\gamma(s) \sin 2\pi\nu_0 - \frac{1}{f} (\cos 2\pi\nu_0 - \alpha(s) \sin 2\pi\nu_0) & \cos 2\pi\nu_0 - \alpha(s) \sin 2\pi\nu_0 \end{pmatrix} \end{aligned}$$

- We calculate the trace to find the new tune

$$\cos 2\pi\nu = \frac{1}{2} \text{Tr}(\mathbf{M}') = \cos 2\pi\nu_0 - \frac{1}{2f} \beta(s) \sin 2\pi\nu_0$$

- For small errors

$$\cos 2\pi(\nu_0 + \Delta\nu) \approx \cos 2\pi\nu_0 - 2\pi \sin 2\pi\nu_0 \Delta\nu = \cos 2\pi\nu_0 - \frac{1}{2f} \beta(s) \sin 2\pi\nu_0$$

$$\Rightarrow \Delta\nu = \frac{1}{4\pi} \frac{\beta(s)}{f}$$



Total Tune Shift

- The focal length associated with a local anomalous gradient is

$$d\left(\frac{1}{f}\right) = \frac{B'}{(B\rho)} ds$$

- So the total tune shift is

$$\Delta \nu = \frac{1}{4\pi} \oint \beta(s) \frac{B'(s)}{(B\rho)} ds$$



Local Correction

- Recall our generic transfer matrix

$$\begin{pmatrix} x_1 \\ x'_1 \end{pmatrix} = \begin{pmatrix} \sqrt{\frac{\beta_1}{\beta_0}} (\cos \Delta\psi + \alpha_0 \sin \Delta\psi) & \sqrt{\beta_0 \beta_1} \sin \Delta\psi \\ \frac{1}{\sqrt{\beta_0 \beta_1}} ((\alpha_0 - \alpha_1) \cos \Delta\psi - (1 + \alpha_0 \alpha_1) \sin \Delta\psi) & \sqrt{\frac{\beta_0}{\beta_1}} (\cos \Delta\psi - \alpha_1 \sin \Delta\psi) \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$

- If we use a dipole to introduce a small bend Θ at one point, it will in general propagate as

$$\begin{pmatrix} x(\Delta\psi) \\ x'(\Delta\psi) \end{pmatrix} = \begin{pmatrix} \sqrt{\frac{\beta(s)}{\beta_0}} (\cos \Delta\psi + \alpha_0 \sin \Delta\psi) & \sqrt{\beta_0 \beta(s)} \sin \Delta\psi \\ \frac{1}{\sqrt{\beta_0 \beta(s)}} ((\alpha_0 - \alpha(s)) \cos \Delta\psi - (1 + \alpha_0 \alpha(s)) \sin \Delta\psi) & \sqrt{\frac{\beta_0}{\beta(s)}} (\cos \Delta\psi - \alpha(s) \sin \Delta\psi) \end{pmatrix} \begin{pmatrix} 0 \\ \theta \end{pmatrix}$$

$$x(\Delta\psi) = \theta \sqrt{\beta_0 \beta(s)} \sin \Delta\psi$$

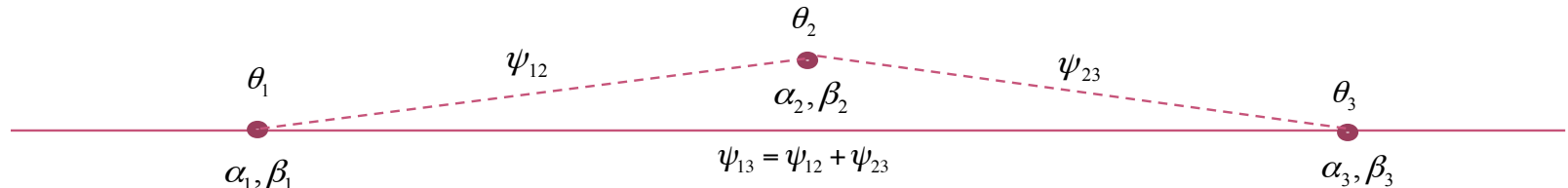
$$x'(\Delta\psi) = \theta \sqrt{\frac{\beta_0}{\beta(s)}} (\cos \Delta\psi - \alpha(s) \sin \Delta\psi)$$

Remember this one forever



“Three Bump”

- Consider a particle going down a beam line. By using a combination of three magnets, we can localize the beam motion to one area of the line



- We require

$$x_3 = \theta_1 \sqrt{\beta_1 \beta_3} \sin \psi_{13} + \theta_2 \sqrt{\beta_2 \beta_3} \sin \psi_{23} = 0$$

$$\Rightarrow \theta_2 = -\theta_1 \sqrt{\frac{\beta_1}{\beta_2}} \frac{\sin \psi_{13}}{\sin \psi_{23}}$$

Local Bumps are an *extremely* powerful tool in beam tuning!!

$$\begin{aligned} \theta_3 &= -\left(\theta_1 \sqrt{\frac{\beta_1}{\beta_3}} (\cos \psi_{13} - \alpha_3 \sin \psi_{13}) + \theta_2 \sqrt{\frac{\beta_2}{\beta_3}} (\cos \psi_{23} - \alpha_3 \sin \psi_{23}) \right) \leftarrow \text{Cancel out angle from first two bends} \\ &= -\theta_1 \left(\sqrt{\frac{\beta_1}{\beta_3}} (\cos \psi_{13} - \alpha_3 \sin \psi_{13}) - \sqrt{\frac{\beta_1}{\beta_2}} \frac{\sin \psi_{13}}{\sin \psi_{23}} \sqrt{\frac{\beta_2}{\beta_3}} (\cos \psi_{23} - \alpha_3 \sin \psi_{23}) \right) \\ &= -\theta_1 \sqrt{\frac{\beta_1}{\beta_3}} \left(\cos \psi_{13} - \frac{\sin \psi_{13}}{\sin \psi_{23}} \cos \psi_{23} \right) = -\theta_1 \sqrt{\frac{\beta_1}{\beta_3}} \left(\frac{\sin \psi_{23} \cos \psi_{13} - \cos \psi_{23} \sin \psi_{13}}{\sin \psi_{23}} \right) = -\theta_1 \sqrt{\frac{\beta_1}{\beta_3}} \left(\frac{\sin(\psi_{23} - \psi_{13})}{\sin \psi_{23}} \right) \end{aligned}$$

$$\Rightarrow \theta_3 = \theta_1 \sqrt{\frac{\beta_1}{\beta_3}} \left(\frac{\sin \psi_{12}}{\sin \psi_{23}} \right)$$



Controls Example

➤ From Fermilab “Acnet” control system

- ◆ The B:xxxx labels indicate individual trim magnet power supplies in the Fermilab Booster
- ◆ Defining a “MULT: *N*” will group the *N* following magnet power supplies
- ◆ Placing the mouse over them and turning a knob on the control panel will increment the individual currents according to the ratios shown in green

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! INJECTION POSITION
MULT      :6
-B:VL5T   [5]*2.45 473 f(t) values      4.933      Amps
-B:VL6T   [5]*1   6 473 f(t) values      2.117      Amps
-B:VL7T   [5]*2.47 473 f(t) values      2.058      Amps
-B:VL5T   *2.4   VL5 473 f(t) values      4.933      Amps
-B:VL6T   *1     VL6 473 f(t) values      2.117      Amps
-B:VL7T   *2.4   VL7 473 f(t) values      2.058      Amps
MULT      :3
-B:VL5T   [1]*2.45 473 f(t) values      5.717      Amps
-B:VL6T   [1]*1   6 473 f(t) values      3.566      Amps
-B:VL7T   [1]*2.47 473 f(t) values      2.561      Amps
MULT      :3
-B:VL5T   [2]*2.45 473 f(t) values      5.642      Amps
-B:VL6T   [2]*1   6 473 f(t) values      .427      Amps
-B:VL7T   [2]*2.47 473 f(t) values      .718      Amps
MULT      :3
-B:VL5T   [3]*2.45 473 f(t) values      20.65      Amps
-B:VL6T   [3]*1   6 473 f(t) values      3.389      Amps
-B:VL7T   [3]*2.47 473 f(t) values      9.95      Amps
MULT      :3
-B:VL5T   [4]*2.45 473 f(t) values      15.21      Amps
-B:VL6T   [4]*1   6 473 f(t) values      6.348      Amps
-B:VL7T   [4]*2.47 473 f(t) values      16.35      Amps
    
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Off-Momentum Particles

- Our previous discussion implicitly assumed that all particles were at the same momentum
 - ◆ Each quad has a constant focal length
 - ◆ There is a single nominal trajectory
- In practice, this is never true. Particles will have a distribution about the nominal momentum
- We will characterize the behavior of off-momentum particles in the following ways
 - ◆ “Dispersion” (D): the dependence of position on deviations from the nominal momentum

$$\Delta x(s) = D_x(s) \frac{\Delta p}{p_0}$$

D has units of length

- ◆ “Chromaticity” (η) : the change in the tune caused by the different focal lengths for off-momentum particles

$$\Delta \nu_x = \xi_x \frac{\Delta p}{p_0} \quad \left(\text{sometimes } \frac{\Delta \nu_x}{\nu_x} = \xi_x \frac{\Delta p}{p_0} \right)$$

- ◆ Path length changes (momentum compaction)

$$\frac{\Delta L}{L} = \alpha \frac{\Delta p}{p}$$



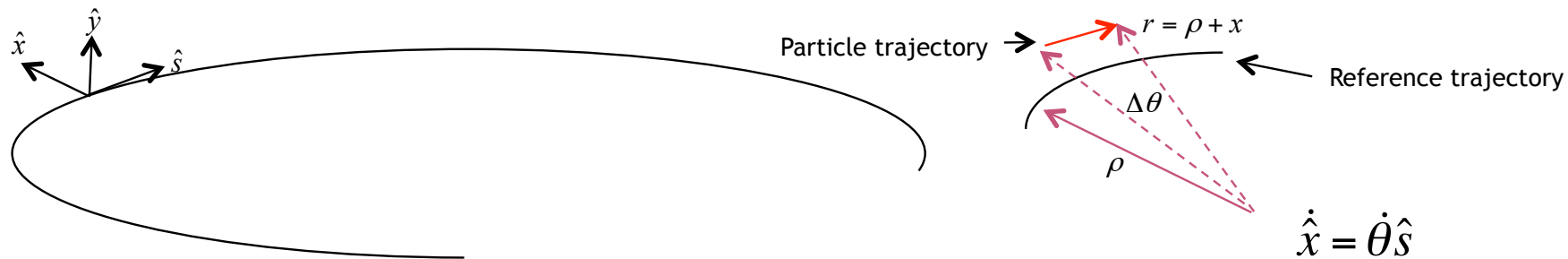
Equations of Motion (redoing the steps we skipped)

- General equation of motion

$$\vec{F} = e\vec{v} \times \vec{B} = \frac{d\vec{p}}{dt} = \frac{d}{dt} \gamma m \vec{R} = \gamma m \ddot{\vec{R}}$$

$$\Rightarrow \ddot{\vec{R}} = \frac{e\vec{v} \times \vec{B}}{\gamma m} = \frac{e}{\gamma m} \begin{vmatrix} \hat{x} & \hat{y} & \hat{s} \\ v_x & v_y & v_s \\ B_x & B_y & 0 \end{vmatrix} = \frac{e}{\gamma m} (-v_s B_y \hat{x} + v_s B_x \hat{y} + (v_x B_y - v_y B_x) \hat{s})$$

- For the moment, we will consider motion in the horizontal (x) plane, with a reference trajectory established by the dipole fields.



$$\dot{\hat{x}} = \dot{\theta} \hat{s}$$

$$\dot{\hat{s}} = -\dot{\theta} \hat{x}$$

- Solving in this coordinate system, we have

$$\vec{R} = r\hat{x} + y\hat{y}$$

$$\dot{\vec{R}} = \dot{r}\hat{x} + r\dot{\hat{x}} + \dot{y}\hat{y} = \dot{r}\hat{x} + r\dot{\theta}\hat{s} + \dot{y}\hat{y}$$

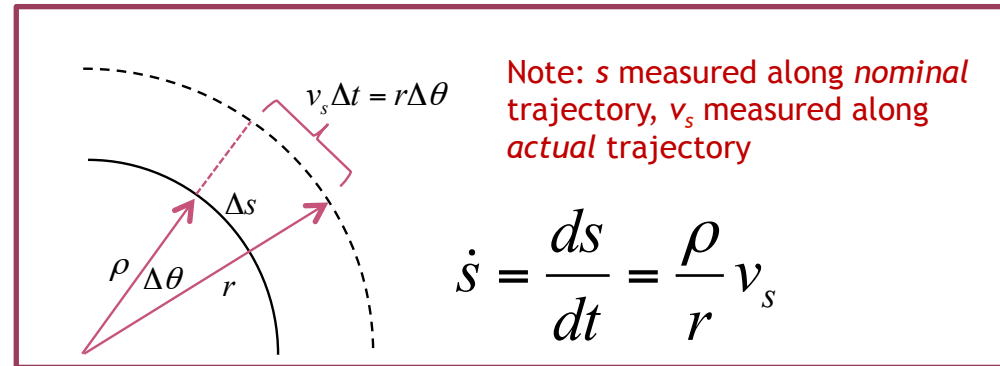
$$\begin{aligned} \ddot{\vec{R}} &= (\ddot{r}\hat{x} + \dot{r}\dot{\hat{x}}) + (\dot{r}\dot{\theta}\hat{s} + r\ddot{\theta}\hat{s} + r\dot{\theta}\dot{\hat{s}}) + \ddot{y}\hat{y} = \ddot{r}\hat{x} + 2\dot{r}\dot{\theta}\hat{s} + r\ddot{\theta}\hat{s} - r\dot{\theta}^2\hat{x} + \ddot{y}\hat{y} \\ &= (\ddot{r} - r\dot{\theta}^2)\hat{x} + (2\dot{r}\dot{\theta} + r\ddot{\theta})\hat{s} + \ddot{y}\hat{y} \end{aligned}$$



Equations of Motion (cont'd)

- Equating the x terms

$$\begin{aligned}\ddot{r} - r\dot{\theta}^2 &= -\frac{ev_s B_y}{\gamma m} \\ &= -\frac{ev_s^2 B_y}{\gamma m v_s} = -\frac{ev_s^2 B_y}{p} \\ &= -\frac{v_s^2 B_y}{(B\rho)}\end{aligned}$$



- Re-express in terms of path length s . Use

$$\frac{d}{dt} = \frac{ds}{dt} \frac{d}{ds} = v_s \frac{\rho}{r} \frac{d}{ds} \Rightarrow \frac{d^2}{dt^2} = \left(v_s \frac{\rho}{r} \right)^2 \frac{d^2}{ds^2}; \quad \dot{\theta} = \frac{v_s}{r}$$

- Rewrite equation

$$\left(v_s \frac{\rho}{r} \right)^2 \frac{d^2 r}{ds^2} - r \left(\frac{v_s}{r} \right)^2 = -\frac{v_s^2 B_y}{(B\rho)}$$

\Rightarrow
(rearrange terms)

$$r'' = -\frac{v_s^2 B_y}{(B\rho)} \frac{r^2}{\rho^2} + \frac{r}{\rho^2}$$

(use $r \Rightarrow \rho + x$)

$$x'' = -\frac{B_y}{(B\rho)} \left(1 + \frac{x}{\rho} \right)^2 + \frac{\rho + x}{\rho^2}; \quad y'' = \frac{B_x}{(B\rho)} \left(1 + \frac{x}{\rho} \right)^2$$



Treating off-momentum Particle Motion

- To treat off-momentum particles, we start with our original these original equations of motion.

$$x'' = -\frac{B_y}{(B\rho)} \left(1 + \frac{x}{\rho}\right)^2 + \frac{\rho + x}{\rho^2}; \quad y'' = \frac{B_x}{(B\rho)} \left(1 + \frac{x}{\rho}\right)^2$$

- The rigidity shown is for the nominal momentum, but I can correct the equation for the true momentum by substituting the “true” rigidity

$$(B\rho)_{true} = (B\rho) \frac{p}{p_0} \rightarrow \frac{1}{(B\rho)_{true}} = \frac{1}{(B\rho)} \frac{p_0}{p} = \frac{1}{(B\rho)} \frac{p_0}{(p_0 + \Delta p)} \approx \frac{1}{(B\rho)} \left(1 - \frac{\Delta p}{p_0}\right)$$

- If we substitute that into the equation, and keep only the lowest order terms, we have

$$x'' = -\frac{B_y}{(B\rho)} \left(1 - \frac{\Delta p}{p_0}\right) \left(1 + \frac{x}{\rho}\right)^2 + \frac{\rho + x}{\rho^2} = (\dots) + \frac{B_y}{(B\rho)} \frac{\Delta p}{p_0} \equiv (\dots) + \frac{B_y}{(B\rho)} \delta$$

$$y'' = \frac{B_x}{(B\rho)} \left(1 - \frac{\Delta p}{p_0}\right) \left(1 + \frac{x}{\rho}\right)^2 = (\dots) - \frac{B_x}{(B\rho)} \delta$$

- If we then also keep only the lowest order terms in the fields, we have

$$B_y = B_0 + B'x \approx B_0; \quad B_x = B'y \approx 0$$

- If we take only the first order terms in the rest of the equation, as we did before, the only change is that extra term on the RHS.

$$x'' + \left(\frac{1}{\rho^2} + \frac{1}{(B\rho)} B' \right) x = \frac{B_0}{(B\rho)} \delta = \frac{1}{\rho} \delta; \quad y'' - \frac{1}{(B\rho)} B' y = 0$$



- This is a second order differential inhomogeneous differential equation, so the solution is

$$x(s) = x_0 C(s) + x'_0 S(s) + \delta d(s)$$

$$x'(s) = x_0 C'(s) + x'_0 S'(s) + \delta d'(s)$$

Where $d(s)$ is the solution particular solution of the differential equation

$$d'' + Kd = \frac{1}{\rho}$$

- We solve this piecewise, for K constant and find

$$K > 0: \quad d(s) = \frac{1}{\rho K} (1 - \cos \sqrt{K} s)$$

$$d'(s) = \frac{1}{\rho \sqrt{K}} \sin \sqrt{K} s$$

$$K < 0: \quad d(s) = -\frac{1}{\rho K} (1 - \cosh \sqrt{K} s)$$

$$d'(s) = \frac{1}{\rho \sqrt{K}} \sinh \sqrt{K} s$$

- Recall

$$x'' + \left(\frac{1}{\rho^2} + B'_y \right) x \Rightarrow K = \left(\frac{1}{\rho^2} + B'_y \right)$$



Matrix Representation

- I have the solution

$$\begin{aligned} x(s) &= x_0 C(s) + x'_0 S(s) + \delta d(s) \\ x'(s) &= x_0 C'(s) + x'_0 S'(s) + \delta d'(s) \end{aligned}$$

Solution to the on-momentum case

Off-momentum correction

- We can express this in matrix form as

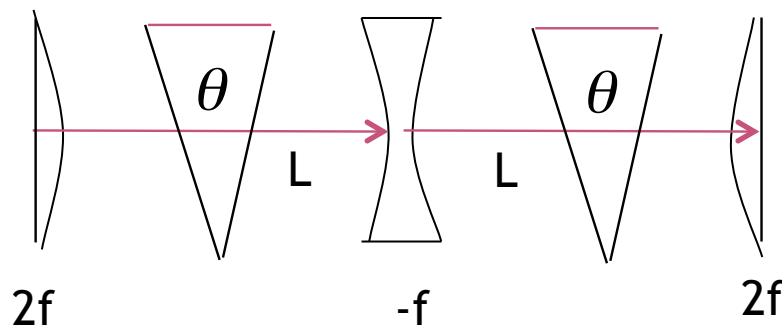
$$\begin{pmatrix} x(s) \\ x'(s) \\ \delta \end{pmatrix} = \begin{pmatrix} \boxed{\begin{matrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{matrix}} & \begin{matrix} d(s) \\ d'(s) \\ 1 \end{matrix} \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \\ \delta \end{pmatrix}$$

Usual transfer matrix



Example: FODO Cell

- We look at our symmetric FODO cell, but assume that the drifts are bend magnets



For a thin lens $d \sim d' \sim 0$. For a pure bend magnet

$$K = \frac{1}{\rho^2} : \quad d(s) = \frac{1}{\rho K} (1 - \cos \sqrt{K} s) = \rho \left(1 - \cos \frac{s}{\rho} \right) \approx \frac{1}{2\rho} s^2 \rightarrow \frac{1}{2} \frac{L^2}{\rho} = \frac{1}{2} \theta L$$

$$d'(s) = \frac{1}{\rho \sqrt{K}} \sin \sqrt{K} s = \sin \frac{s}{\rho} \approx \frac{s}{\rho} \rightarrow \theta$$

Leading to the transfer Matrix

$$M = \begin{pmatrix} 1 & 0 & 0 \\ -\frac{1}{2f} & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & L & \frac{L\theta}{2} \\ 0 & 1 & \theta \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ \frac{1}{f} & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & L & \frac{L\theta}{2} \\ 0 & 1 & \theta \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ -\frac{1}{2f} & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} 1 - \frac{L^2}{2f^2} & 2L \left(1 + \frac{L}{2f} \right) & 2L\theta \left(1 + \frac{L}{4f} \right) \\ -\frac{L}{2f^2} + \frac{L^2}{4f^3} & 1 - \frac{L^2}{2f^2} & 2\theta \left(1 - \frac{L}{4f} - \frac{L^2}{8f^2} \right) \\ 0 & 0 & 1 \end{pmatrix}$$



Solving for Equilibrium Orbit

- We hypothesize that we will have a new equilibrium reference orbit for off-momentum particles, defined as a function of position by

$$x(s, \delta) = D_x(s) \delta$$

“Dispersion”

- We expect this to have the periodicity of the lattice, so in general

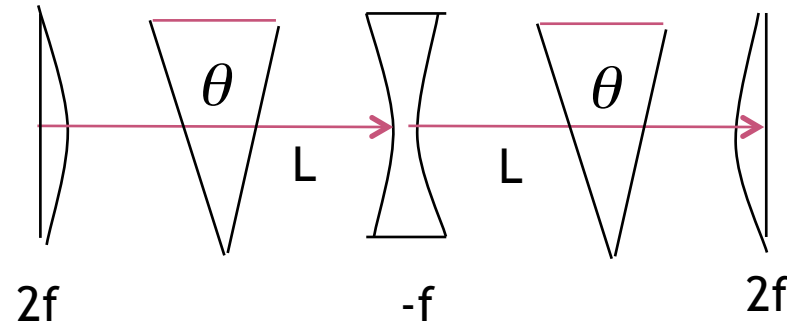
$$\begin{pmatrix} \delta D_x \\ \delta D'_x \\ \delta \end{pmatrix} = \begin{pmatrix} \cos \mu + \alpha \sin \mu & \beta \sin \mu & d \\ -\gamma \sin \mu & \cos \mu - \alpha \sin \mu & d' \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \delta D_x \\ \delta D'_x \\ \delta \end{pmatrix}$$

Can set δ to 1



Solving for Dispersion

- Going back to our original FODO cell (with bends)



- We must solve

$$\begin{pmatrix} D \\ D' \\ 1 \end{pmatrix} = \begin{pmatrix} 1 - \frac{L^2}{2f^2} & 2L\left(1 + \frac{L}{2f}\right) & 2L\theta\left(1 + \frac{L}{4f}\right) \\ -\frac{L}{2f^2} + \frac{L^2}{4f^3} & 1 - \frac{L^2}{2f^2} & 2\theta\left(1 - \frac{L}{4f} - \frac{L^2}{8f^2}\right) \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} D \\ D' \\ 1 \end{pmatrix}$$



Solving for Lattice Functions

- We have already solved for the basic lattice functions

$$\sin \frac{\mu}{2} = \frac{L}{2f}$$

$$\beta_{F,D} = \frac{2L \left(1 \pm \sin \frac{\mu}{2} \right)}{\sin \mu}$$

- You'll solve in the homework

$$D_{F,D} = \frac{\theta L \left(1 \pm \frac{1}{2} \sin \frac{\mu}{2} \right)}{\sin^2 \frac{\mu}{2}}$$

- It will really simplify things if you invoke symmetry to show that

$$\alpha_{F,D} = D'_{F,D} = 0$$

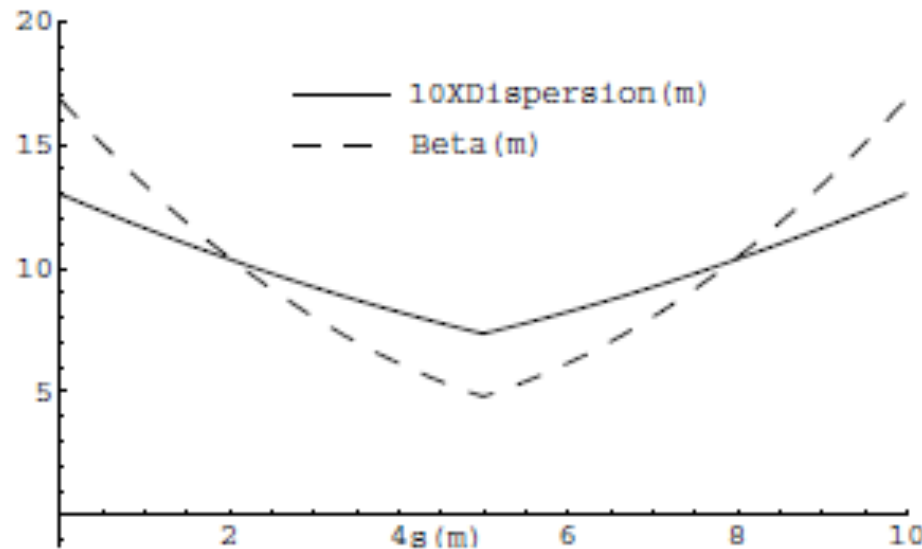


Evolution of Dispersion Functions

- Since the dispersion functions represent displacements, they will evolve like the position

$$\begin{pmatrix} D_x(s) \\ D'_x(s) \\ 1 \end{pmatrix} = \begin{pmatrix} m_{11} & m_{12} & d(s) \\ m_{21} & m_{22} & d'(s) \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} D_x(0) \\ D'_x(0) \\ 1 \end{pmatrix}$$

- Putting it all together





Momentum Compaction and Slip Factor

- In general, particles with a high momentum will travel a longer path length. We have

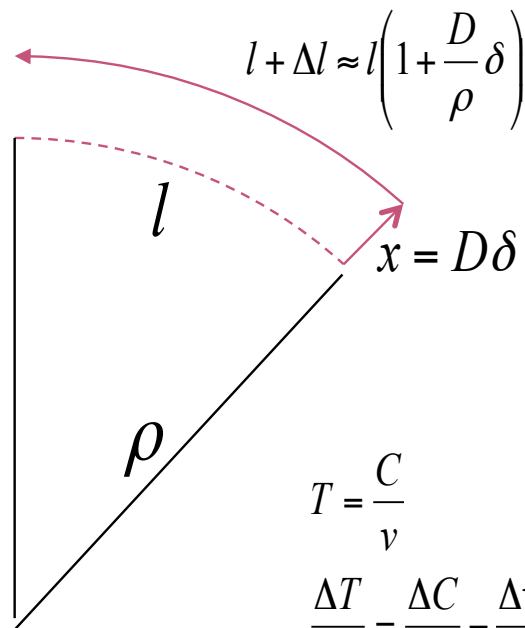
$$C(p_0) = \oint ds$$

$$C(p_0 + \Delta p) = \oint \left(1 + \frac{D}{\rho} \frac{\Delta p}{p_0} \right) ds$$

$$\frac{\Delta C}{C} = \frac{\oint \frac{D}{\rho} ds}{\oint ds} \delta = \left\langle \frac{D}{\rho} \right\rangle \delta$$

“momentum compaction”

$$\equiv \alpha \delta$$



- The slip factor is defined as the fractional change in the orbital period
- Note that

$\gamma < \gamma_T : \quad \eta < 0$ higher energy particles take *less* time to go around
 $\gamma > \gamma_T : \quad \eta > 0$ higher energy particles take *more* time to go around
 $\gamma = \gamma_T : \quad \eta = 0$ "transition"

$$\begin{aligned}
 T &= \frac{C}{v} \\
 \frac{\Delta T}{T} &= \frac{\Delta C}{C} - \frac{\Delta v}{v} = \frac{\Delta C}{C} - \frac{\Delta \beta}{\beta} \\
 &= \alpha \frac{\Delta p}{p} - \frac{1}{\gamma^2} \frac{\Delta p}{p} \\
 &= \left(\frac{1}{\gamma_T^2} - \frac{1}{\gamma^2} \right) \frac{\Delta p}{p} \\
 &\equiv \eta \frac{\Delta p}{p}
 \end{aligned}$$



Transition γ

- In homework, you showed that for a simple FODO CELL

$$\beta_{\max, \min} = 2L \frac{\left(1 \pm \sin \frac{\mu}{2}\right)}{\sin \mu}; \text{ and } D_{\max, \min} = \theta L \frac{\left(1 \pm \frac{1}{2} \sin \frac{\mu}{2}\right)}{\sin^2 \frac{\mu}{2}}$$

- If we assume they vary ~linearly between maxima, then for small μ

$$\langle \beta \rangle \approx \frac{2L}{\mu}; \quad \langle D \rangle \approx \frac{4\theta L}{\mu^2} = 4 \frac{L^2}{\mu^2 \rho} = \frac{\langle \beta \rangle^2}{\rho}$$

- It follows

$$\nu \approx \frac{R}{\langle \beta \rangle} \approx \frac{\rho}{\langle \beta \rangle} \Rightarrow \langle D \rangle \approx \frac{\rho}{\nu^2}$$

$$\alpha_C = \frac{1}{C} \oint \frac{D}{\rho} ds \approx \frac{1}{\rho} \langle D \rangle \approx \frac{1}{\nu^2}$$

$$\gamma_t = \frac{1}{\sqrt{\alpha_C}} \approx \nu$$

- This approximation generally works better than it should



Chromaticity

- In general, momentum changes will lead to a tune shift by changing the effective focal lengths of the magnets
- As we are passing through a magnet, we can find the focal length as

$$\frac{1}{f_0} = \int_0^L \frac{B'}{(B\rho)} ds$$

- But remember that our general equation of motion is

$$x'' + \left(\frac{1}{\rho^2} + \frac{B'(s)}{(B\rho)} \right) x = 0 \equiv x'' + K(s)x$$

- Clearly, a change in momentum will have the same effect on the entire focusing term, so we can write in general

$$\xi = -\frac{1}{4\pi} \oint \beta_0(s) K(s) ds$$

- This can be expressed in terms of lattice functions (after a lot of messy algebra) as

$$\xi = -\frac{1}{4\pi} \oint (\gamma(s) + \alpha'(s)) ds$$

$$\begin{aligned} \frac{1}{f} &= \frac{B'l}{(B\rho)} = \frac{B'l}{(B\rho)_0} \frac{p_0}{p} \approx \frac{1}{f_0} \left(1 - \frac{\Delta p}{p_0} \right) \\ \Delta \frac{1}{f} &= -\frac{1}{f_0} \frac{\Delta p}{p_0} \\ \Rightarrow \Delta \nu &= -\frac{1}{4\pi} \sum_i \beta_i \frac{1}{f_i} \frac{\Delta p}{p_0} \equiv \xi \frac{\Delta p}{p_0} \end{aligned}$$



Chromaticity and Sextupoles

- we can write the field of a sextupole magnet as

$$B(x) = \frac{1}{2} B'' x^2 \quad \left(\text{often expressed } b_2 x^2 \right)$$

- If we put a sextupole in a dispersive region then off momentum particles will see a gradient

$$B'(x = D\delta) \approx B'' D \frac{\Delta p}{p_0}$$

which is effectively like a position dependent quadrupole, with a focal length given by

$$\frac{1}{f_{\text{eff}}} = \frac{B''}{(B\rho)} LD \frac{\Delta p}{p_0}$$

- So we write down the tune-shift as

$$\Delta\nu = \frac{1}{4\pi} \beta \frac{1}{f_{\text{eff}}} = \frac{1}{4\pi} \frac{\beta B''}{(B\rho)} LD \frac{\Delta p}{p_0} \equiv \xi \frac{\Delta p}{p_0}$$

$$\Rightarrow \xi_s = \frac{1}{4\pi} \frac{\beta B''}{(B\rho)} LD$$

- Note, this is only valid when the motion due to momentum is large compared to the particle spread (homework problem)

